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ABSTRACT

Simultaneously measured DD, DT, and D³He reaction histories are used to probe the impacts of multi-ion physics during the shock phase of inertial confinement fusion implosions. In these relatively hydrodynamiclike (burn-averaged Knudsen number $\langle N_K \rangle \sim 0.3$) shock-driven implosions, average-ion hydrodynamic DUEd simulations are able to reasonably match burnwidths, nuclear yields, and ion temperatures. However, kinetic-ion FPION simulations are able to better simulate the timing differences and time-resolved reaction rate ratios between DD, DT, and D³He reactions. FPION simulations suggest that the D³He/DT reaction rate ratio is most directly impacted by ion species separation between the ³He and T ions, whereas the D³He/DD reaction rate ratio is affected by both ion species separation and ion temperature decoupling effects.

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I. INTRODUCTION

Strong shock propagation plays an important role in energy transport in many astrophysical phenomena¹ and during the shock phase of inertial confinement fusion (ICF) implosions.² Average-ion, radiation-hydrodynamic codes^{3,4} are typically used to model ICF implosions, but they only model an averaged ion species and assume a collisional plasma. The interactions between different ion species and deviations from hydrodynamic evolution are more pronounced during the shock phase of an ICF implosion, when ion-ion mean paths in the fuel are comparable to the fuel radius. Multi-ion and kinetic physics can lead to measurable changes in implosion performance such as yield degradation,⁵ anomalous yield scaling,^{6,7} ion thermal decoupling,⁸ and ion species separation.^{9,10} These multi-ion/kinetic effects related to the ion mean free path,¹¹ ion mass,¹² and ion charge¹³ have been modeled using reduced ion-kinetic models,¹⁴ particle-in-cell (PIC) simulations,^{15–17} and kinetic-ion simulations.^{18–22}

This work follows the experiments described by Sio *et al.*,¹⁰ and greatly expands on this previous work through the inclusion of (1) two new experiments on DD and D³He reaction histories, (2) one new experiment on DD, DT, and D³He reaction histories, and (3) kinetic-ion FPION simulations in the interpretation of the data. There are

significant experimental challenges in diagnosing the density and temperature differences between different ion species (ion species separation and ion thermal decoupling, respectively). With few exceptions,^{10,23} the majority of existing experimental work investigating the role of kinetic and multi-ion physics in ICF implosions made use of time-integrated nuclear observables (reaction yields and ion temperatures). The experimental interaction signatures between the D, T, and ³He ions are the DD, DT, and D³He reactions and measurements of the DD, DT, and D³He reaction histories using the Particle X-ray Temporal Diagnostic (PXTD)²⁴ enable time-resolved studies of these multi-ion effects. In this work, time-resolved DD, DT, and D³He reaction rates are used to probe the underlying changes in the plasma's temperature and density profiles and are compared with average-ion DUEd⁴ and kinetic-ion FPION¹⁹ simulations. These measurements during the ICF shock phase are affected by kinetic/multi-ion physics which cannot be accounted for in average-ion-fluid simulations.

This paper is organized as follows: Sec. II describes the experimental setup and diagnostics. Section III compares the measured data with average-ion and kinetic-ion simulations. Section IV discusses interpretation of the data. Section V summarizes the main results and outlines future work.

II. OMEGA EXPERIMENTS

The experiments described in this work are performed on the 60-beam OMEGA laser facility.²⁵ The targets are spherical and approximately 860 μm in outer diameter, with a thin SiO_2 shell of thickness between 2.2 and 2.7 μm . These targets are filled with different mixtures of D_2 , ^3He , and T_2 gas and imploded symmetrically using 60 beams with a laser energy of $\sim 14\text{ kJ}$ (at a wavelength of 351 nm) using a 0.6-ns-square pulse shape. The trace amount of tritium in the gas fill provides additional diagnostic measurements (DT yield, ion temperature, and reaction history) without perturbing the implosion. The symmetry of the implosion is improved by phase plates, polarization smoothing, and smoothing by spectral dispersion. In this type of shock-driven implosion (so called because nuclear yields are dominated by shock heating rather than compression), the thin shell is mostly ablated away by the laser, and the implosion begins to disassemble when the rebounding shock reaches the fuel-shell interface. These implosions are ideal for studying ICF shock phase dynamics because they mimic the plasma conditions during the shock phase of more complicated ICF implosions.⁵

In the experiments, DD and DT yields and ion temperatures are measured by neutron time-of-flight²⁶ diagnostics. The D^3He yield and ion temperature are measured using Wedge-Range-Filter proton spectrometers²⁷ and Charged Particle Spectrometers.²⁸ The laser absorption (measured using a Full Aperture Back Scatter²⁹ system) and fuel-shell trajectory (measured using X-ray framing cameras³⁰) are used to constrain postshot simulations. The primary observables—DD, DT, and D^3He reaction histories—are simultaneously measured using the Particle X-ray Temporal Diagnostic (PXTD)²⁴ with high relative timing precision (~ 10 ps). On some shots, the Neutron Temporal

Diagnostic³¹ provided independent measurements of the DD and/or DT reaction histories.

Data from four shock-driven implosion experiments are discussed in this work, and representative PXTD streak images from the experiments are shown in Fig. 1. The targets and laser drives for all four experiments are approximately the same, but the gas fills are different. These implosions have a burn-averaged Knudsen number ($\langle N_K \rangle \sim 0.3$, defined as the burn-averaged ion mean free path (λ_{ii}) over the fuel radius (R_{burn})). PXTD is a scintillator-based, streaked emission history diagnostic, and each of the three scintillator channels is sensitive to X-rays, charged particles, and/or neutrons depending on filtering. The horizontal axis of the streak image is the time axis, and each streak image has either two or three independent scintillator signals (different color lineouts in Fig. 1). Because of the long scintillator decay time (~ 1.2 ns), the implosion reaction history of interest is encoded in the rising edge of the scintillator signal. The reaction history is extracted using a deconvolution or forward-fitting procedure to remove the instrumental response, transit time broadening in the scintillator, and Doppler broadening. The relative timing uncertainty is ± 10 ps between D^3He and DT reaction histories. Doppler broadening (a function of diagnostic insertion distance) impacts the DD reaction history more strongly. When the DD reaction history is measured, the relative timing uncertainties are ± 20 ps when PXTD is fielded at 9 cm away from the implosion [Fig. 1(a)] and 110 ps when PXTD is fielded at 3 cm away from the implosion [Fig. 1(c)].

The timing difference between the signals on the streak image is related to the times of flight to the detector for different particles. As an example, for a detector at 9 cm away from the target, times of flight

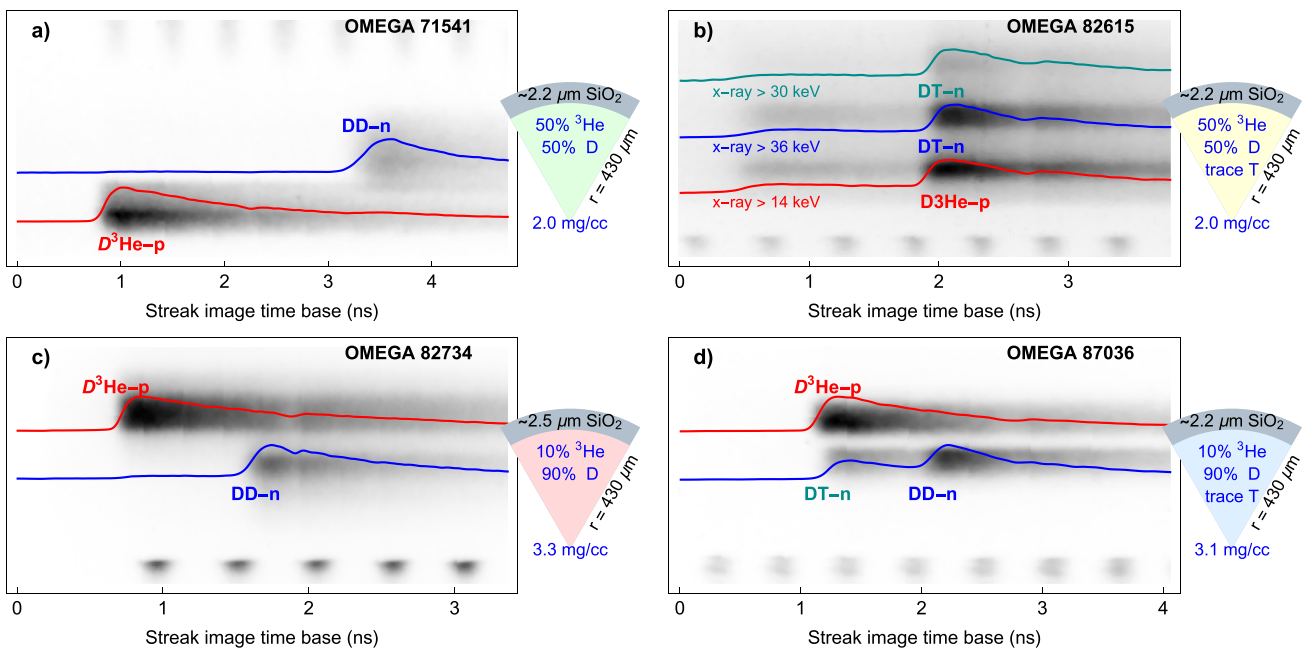


FIG. 1. Representative PXTD streak data, showing (a) DD-n and $\text{D}^3\text{He-p}$ signals in a 50%–50% D^3He -gas-filled implosion, (b) DT-n and $\text{D}^3\text{He-p}$ signals in a 50%–50% D^3He -gas-filled (with trace T) implosion, (c) DD-n and $\text{D}^3\text{He-p}$ signals in a 90%–10% D^3He -gas-filled implosion, and (d) DD-n, DT-n, and $\text{D}^3\text{He-p}$ signals in a 90%–10% D^3He -gas-filled (with trace T) implosion. All the gas-fill compositions indicate the atomic percentage. PXTD was fielded at 9 cm away from the target for (a) and (b) and at 3 cm away from the target for (c) and (d).

for DD-n, DT-n, and D³He-p are ~ 4.18 ns, 1.78 ns, and 1.74 ns, respectively. These flight times are determined by the birth energies of the particles as well as the measured ion temperatures,³² and for the D³He-p, they are assessed through measurements of the D³He-p energy spectrum. More details of the PXTD diagnostic and analysis are discussed in the instrumentation paper.²⁴

The first experiment [Fig. 1(a)] has a 50%–50% D³He gas fill, and PXTD measured DD and D³He reaction histories. The second experiment [Fig. 1(b)] has a 50%–50% D³He gas fill (with trace T), and PXTD measured DT and D³He reaction histories, as well as X-ray emission histories from the implosion. The X-ray signals and the nuclear signals are separated in time on the streak image because of their different flight times to the detector. The third experiment [Fig. 1(c)] has a 90%–10% D³He gas fill, and PXTD measured DD and D³He reaction histories. The fourth experiment [Fig. 1(d)] used an optimized 90%–10% D³He gas fill (with trace T) that enabled PXTD to measure DD, DT, and D³He reaction histories. All gas-fill compositions indicate the atomic percentage.

III. DATA AND SIMULATION COMPARISONS

Average-ion hydrodynamic code DUED⁴ and Vlasov-Fokker-Planck kinetic-ion code FPION¹⁹ are used to provide further insight into the PXTD data. DUED solves the mass and momentum equations for one averaged ion fluid and separates energy equations for electrons and ions. It includes collisional transport processes (electron-ion coupling, flux-limited electron, and ion conductivities), equations of state, ion viscosity, and multigroup diffusion for radiation. DUED uses the measured laser power for postshot simulations, and adjustment to laser absorption has only a small impact on observables. Two other average-ion hydrodynamic codes LILAC³³ and HYADES³⁴ have also been used to simulate these implosions with similar results although DUED has the best overall agreement with the measured observables.

FPION implements the Vlasov-Fokker-Planck equations for an arbitrary number of ion species in spherical geometry, treating the lighter fuel ions kinetically and the heavier SiO₂ shell ions (which are expected to be close to local thermal equilibrium) as a fluid. Initializing from average-ion-fluid simulation results, this hybrid kinetic-fluid approach allows treatment of both kinetic ions in the fuel and diffusion across the fuel-shell interface. FPION has been used to simulate similar shock-driven implosions, and more details on the simulation methods are described in Ref. 19.

Figures 2 and 3 summarize the DD, DT, and D³He nuclear yields, ion temperatures, burnwidths, and differences in nuclear bang times as measured by PXTD and as simulated by DUED and FPION. The bang time is the time of peak nuclear emission. In particular, Fig. 3(a) shows the yield over simulated (YOS) values, calculated as the experimental yield, and divided by either the DUED-simulated or FPION-simulated yield.

Averaging over all four implosion classes and the DD, DT, and D³He reactions, DUED overpredicts yields by 90%, whereas FPION underpredicts yields by 10%. DUED is able to better match the measured ion temperatures (on average, 1.1 standard deviations away, vs 2.1 standard deviations away for FPION). However, DUED is worse at matching the measured burnwidths (on average, 1.3 standard deviations away, vs 0.9 standard deviations away for FPION). FPION is able to better match the timing differences between reaction

histories as compared to DUED although they are still smaller than the measurements.

Four classes of implosions from four different experiments are represented in Figs. 2 and 3. In considering the different experiments, implosions with and without trace T should be considered similar, but not nominally identical, because of systematic differences in targets (shell thickness, etc.) between experiments. For example, a discrepancy is observed for the two implosion types at higher fill density. The increase in the D³He yield between the implosion types is likely due to the difference in the target thickness, rather than the addition of trace tritium. It is puzzling that FPIONs yield very good agreement for D³He becomes worse with the addition of trace tritium, as differences in target and laser parameters between implosions are taken into account in the simulations.

Figure 4 shows the DD, DT, and D³He reaction histories as measured by PXTD and as simulated by DUED and FPION, for the cases of DD/D³He reaction histories [Fig. 4(a)], DT/D³He reaction histories [Fig. 4(b)], and DD/DT/D³He reaction histories [Fig. 4(c)]. In the DUED simulations, the DD, DT, and D³He reaction histories rise at almost the same time within 10 ps. However, in the PXTD data, the timing difference between the DT and D³He reaction histories and the timing difference between the DD and D³He histories are on the order of 40–50 ps, well outside the measurement uncertainty of ± 10 ps. Section IV will discuss in more detail the potential mechanisms leading to the differences in these reaction histories. Overall, kinetic-ion FPION simulations are better able to capture the relative timing and reaction rate ratios between DD, DT, and D³He reactions as compared to the average-ion DUED simulations. FPION-simulated reaction histories also show the same qualitative behaviors as the reaction histories simulated using the Particle-in-Cell code LSP,¹⁰ although FPION is able to better match all the time-integrated and time-resolved measurements.

An important observation is that the DUED-simulated DD and DT reaction histories in these shock-driven implosions [Fig. 4(c)] have almost identical shapes. The similarity between the DD and DT reaction histories is a consequence of the average-ion-fluid assumption in the simulation and the nearly flat DT/DD reactivity ratio near the ion temperature of ~ 10 keV (Fig. 5). That is, any observed difference between the DD and DT reaction histories in this temperature range [as we see in Fig. 4(c)] is a direct observation of nonaverage-ion-fluid effects.

As there is no significant difference in the measured ion temperatures, burnwidths, and timing differences between implosions with 50%–50% D³He vs implosions with 90%–10% D³He and as the observables are repeatable for the same implosion type (Table I in the Appendix), the discussions in the Sec. IV will focus on 90%–10% D³He (with trace T) implosions for which DD, DT, and D³He histories are simultaneously measured.

IV. DISCUSSION

Strong shock propagation is inherently a kinetic phenomenon,²⁰ and can drive differences in ion densities and temperatures (ion species separation and ion temperature decoupling, respectively) in a multi-ion plasma mixture with different masses and charges. FPION simulations for a representative 90%–10% D³He (with trace T) shock-driven implosion are used in this section. Figure 6 shows the FPION ion density and temperature radial profiles for the D, T, and ³He ions

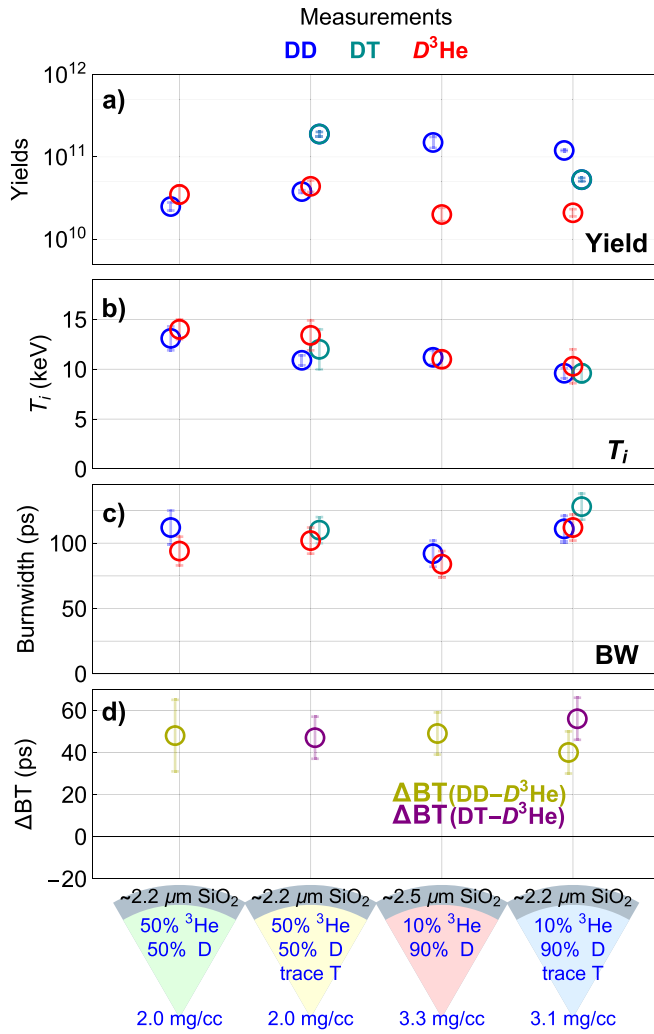


FIG. 2. Measured, averaged (a) nuclear yields, (b) reaction temperatures, (c) burnwidths, and (d) differences in the bang time (time of peak nuclear emission) for four different classes of D³He-gas-filled (with or without trace T) implosions. Each data point is averaged over 2–4 nominally identical shots. The complete data table is available in the [Appendix \(Table I\)](#).

at $t = 0.56$ ns [Figs. 6(a) and 6(b)] and at $t = 0.69$ ns [Figs. 6(c) and 6(d)]. As the strong shock propagates inward at $t = 0.56$ ns, ion density and temperature differences have already developed between the D, T, and ³He ions. The T ions are lagging behind the shock front, and the ³He ions have developed higher temperature than the D ions because of the differences in masses and charges. Later during shock rebound at $t = 0.69$ ns near the nuclear bang times, these density and temperature differences that evolved during shock convergence have developed into higher ³He ion concentrations and higher ³He and T ion temperatures in the central region of the fuel.

Figure 7 shows density plots of the fractional changes in the (a) ³He/D fuel ratio and (b) ³He/T ratio from the initial fuel ratio, as well as the temperature ratio between (c) ³He and D ions and (d) ³He and T ions. In the density plots, the shock converges at the center at

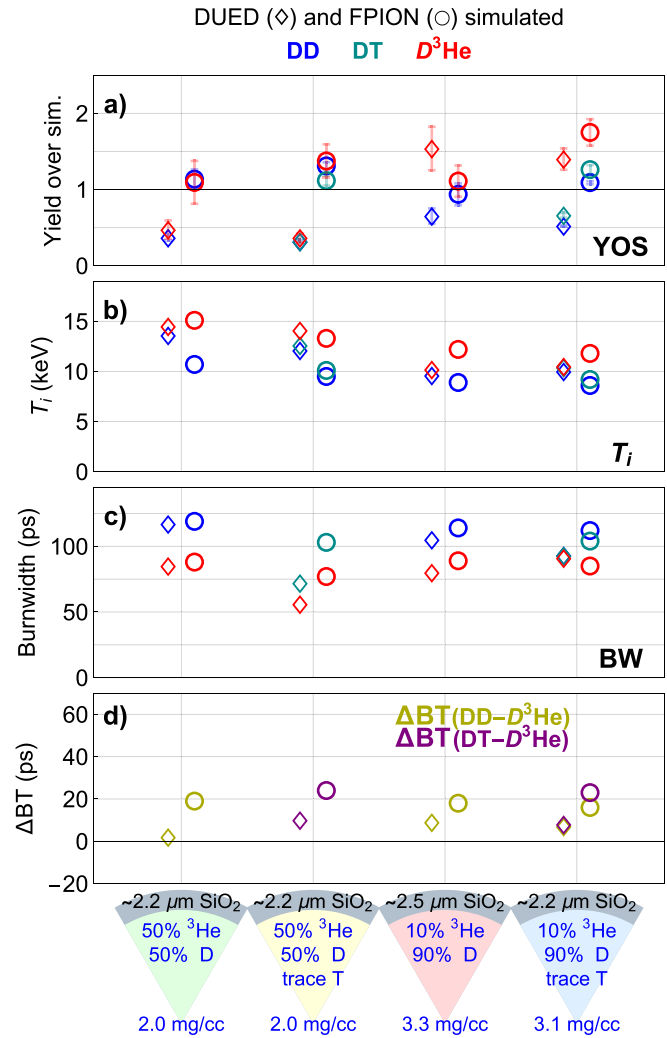


FIG. 3. (a) Measured nuclear yields over simulated (YOS), (b) reaction temperatures, (c) burnwidths, and (d) differences in bang time (time of peak nuclear emission) for four different classes of D³He-gas-filled (with or without trace T) implosions as simulated by DUED (◇) and FPION (○). The complete data table is available in the [Appendix \(Table I\)](#).

~0.6 ns, and the nuclear bang times are ~0.7 ns. It is easier to observe in these density plots the higher ³He/D and ³He/T fuel ratio relative to the initial gas-fill ratio near the bang time, as well as the higher ³He and T ion temperatures relative to the D ions.

In turn, these deviations from average-ion density and temperature profiles of the D, T, and ³He ions translate into changes in the DD, DT, and D³He reaction rates. For a nuclear reaction involving two Maxwellian ion populations at two different temperatures, the effective fusion temperatures³⁵ for the DD, DT, and D³He reactions are given by

$$T_{fusion,DD} = T_{i,D}, \quad (1)$$

$$T_{fusion,DT} = \frac{m_T T_{i,D} + m_D T_{i,T}}{m_D + m_T}, \quad (2)$$

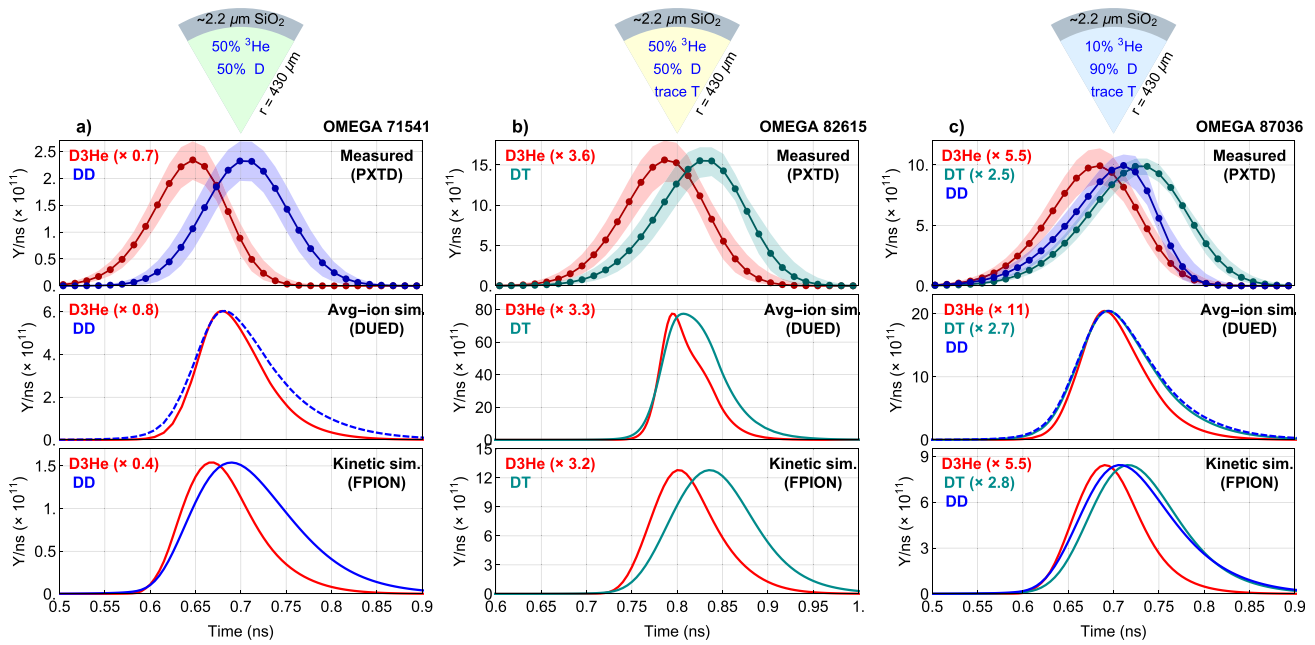


FIG. 4. Comparison between PXTD data, average-ion DUED simulation, and kinetic-ion FPION simulation for (a) DD and $D^3\text{He}$ reaction histories in a 50%–50% $D^3\text{He}$ -gas-filled implosion, (b) DT and $D^3\text{He}$ reaction histories in a 50%–50% $D^3\text{He}$ -gas-filled (with trace T) implosion, and (c) DD, DT, and $D^3\text{He}$ reaction histories in a 90%–10% $D^3\text{He}$ -gas-filled (with trace T) implosion. DD, DT, and $D^3\text{He}$ reaction histories are shown in blue, teal, and red, respectively. The absolute time axis is shifted within the measurement uncertainty to better compare with simulations visually. Graphics in (b) are adapted with permission from Sio *et al.* Phys. Rev. Lett. **122**, 035001 (2019). Copyright 2019 American Physical Society.

$$T_{\text{fusion}, D^3\text{He}} = \frac{m^3_{\text{He}} T_{i,D} + m_D T_{i,^3\text{He}}}{m_D + m^3_{\text{He}}}, \quad (3)$$

where m and T_i are the masses and ion temperatures of the D, T, and ^3He ions.

To illustrate how density and temperature differences between ion species can give rise to differences in reaction histories and reaction rate ratios, let us consider several different ways that reaction rates can be calculated. If $n_{i,D}$, $n_{i,T}$, and $n_{i,^3\text{He}}$ are fixed to the initial fuel ratio and $T_{i,D} = T_{i,T} = T_{i,^3\text{He}}$, the average-ion approximation ($\langle n_i \rangle$, $\langle T_i \rangle$) for the $D^3\text{He}$ reaction history is given by

$$Y_{D^3\text{He}}^{\text{avg ion}}(t)/s = \int_{D,0}^{f_{D,0}} \int_{He,0}^{f_{He,0}} \langle n_i \rangle^2 \langle \sigma v \rangle_{D^3\text{He}} \langle T_i \rangle dV, \quad (4)$$

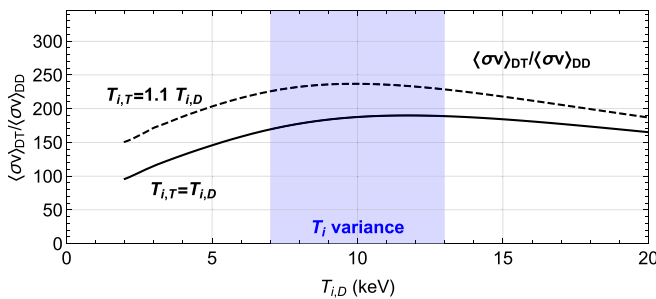


FIG. 5. DT/DD reactivity ratio as a function of deuteron ion temperature if $T_{i,T} = T_{i,D}$ (black) and if $T_{i,T} = 1.1 T_{i,D}$ (black-dashed). The shaded blue region is the burn-weighted temperature variance (from simulation) for a representative shock-driven implosion discussed in this work.

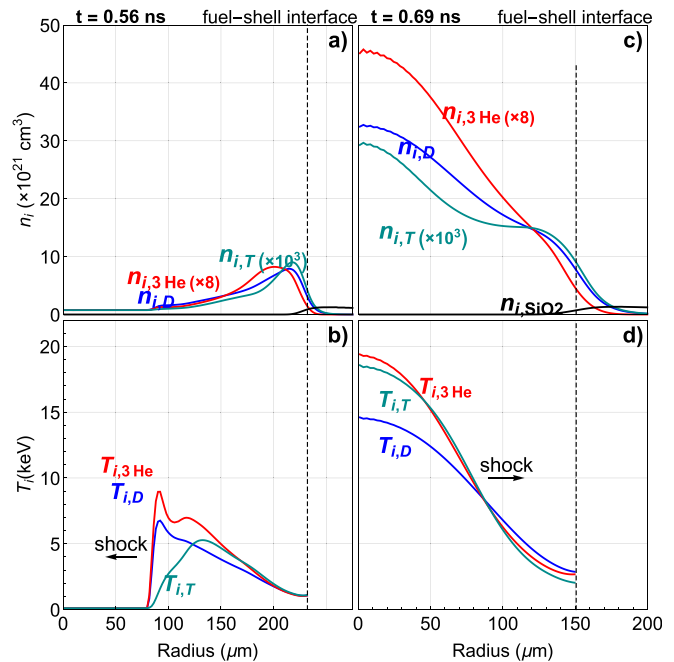


FIG. 6. Kinetic FPION simulation of a 90%–10% $D^3\text{He}$ -gas-filled (with trace T) shock-driven implosion, showing density profiles and temperature profiles at $t = 0.56$ ns during shock convergence (a) and (b) and at $t = 0.69$ ns during shock rebound (c) and (d). The ^3He and T ion densities are scaled to the initial D ion density. Fuel and shell ions can diffuse across the fuel-shell interface (black-dashed line).

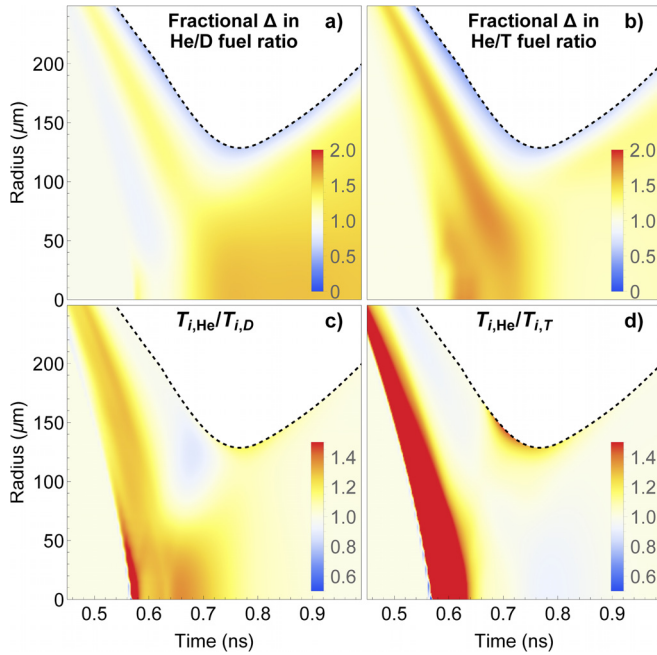


FIG. 7. Kinetic FPION simulation of a 90%–10% $D^3\text{He}$ -gas-filled (with trace T) shock-driven implosion, showing (a) fractional change in the $^3\text{He}/D$ fuel ratio from the initial fuel ratio, (b) fractional change in the $^3\text{He}/T$ fuel ratio from the initial fuel ratio, (c) temperature ratio between ^3He and D ions, and (d) temperature ratio between ^3He and T ions. Fuel and shell ions can diffuse across the fuel-shell interface (black-dashed line).

where $f_{D,0}$ and $f_{^3\text{He},0}$ are the initial fill fraction for D and ^3He , respectively. $\langle n_i \rangle$ and $\langle T_i \rangle$ are the averaged ion density and temperature, and $\langle \sigma v \rangle$ is the Maxwellian-averaged reactivity.

If the density profiles are fixed, but different temperatures between the ions are permitted ($\langle n_i \rangle$, $T_{i,D}$, $T_{i,T}$, $T_{i,^3\text{He}}$), the $D^3\text{He}$ reaction history is given by

$$Y_{D^3\text{He}}^{\text{avg } n_i}(t)/s = \int f_{D,0} f_{^3\text{He},0} \langle n_i \rangle^2 \langle \sigma v \rangle_{D^3\text{He}}(T_{i,D}, T_{i,^3\text{He}}) dV. \quad (5)$$

If the density profiles are allowed to vary, but temperatures between the ions are fixed ($n_{i,D}$, $n_{i,T}$, $n_{i,^3\text{He}}$, $\langle T_i \rangle$), the $D^3\text{He}$ reaction history is given by

$$Y_{D^3\text{He}}^{\text{avg } T_i}(t)/s = \int n_{i,D} n_{i,^3\text{He}} \langle \sigma v \rangle_{D^3\text{He}}(\langle T_i \rangle) dV. \quad (6)$$

Finally, when each ion species may have different temperature and density profiles ($n_{i,D}$, $n_{i,T}$, $n_{i,^3\text{He}}$, $T_{i,D}$, $T_{i,T}$, $T_{i,^3\text{He}}$), the $D^3\text{He}$ reaction history given by

$$Y_{D^3\text{He}}^{\text{multi ion}}(t)/s = \int n_{i,D} n_{i,^3\text{He}} \langle \sigma v \rangle_{D^3\text{He}}(T_{i,D}, T_{i,^3\text{He}}) dV. \quad (7)$$

Simultaneously measured DD, DT, and $D^3\text{He}$ reaction histories provide an unprecedented opportunity to compare time-resolved $D^3\text{He}/DT$, $D^3\text{He}/DD$, and DT/DD reaction rate ratios with average-ion-fluid calculations [Eq. (4)] from DUED simulations, postprocessed multi-ion-fluid calculations [Eq. (7)] from FPION simulations, and kinetic calculations

from FPION simulations. These comparisons are summarized in Fig. 8. In the case of the $D^3\text{He}/DT$ [Fig. 8(a)] and $D^3\text{He}/DD$ [Fig. 8(b)] reaction rate ratios, FPION calculations, kinetic or reduced to multi-ion-fluid, agree much better with the measurements as compared to DUED. The difference between the kinetic and the multi-ion-fluid FPION calculations (purple vs purple-dashed) is also modest, which reflects the hydrodynamiclike ($\langle N_K \rangle \sim 0.3$) plasma conditions in these implosions.

Figure 8(c) shows higher-than-expected measured DT/DD reaction rate ratios at late time, which is not explained by DUED nor FPION. This can also be seen in Fig. 4(c) as a longer measured DT burn relative to DD . One possible explanation for the observation may be higher-than-expected deuteron diffusion out of the burn region relative to tritons, which will decrease the DD reaction rate relative to DT .

However, the multi-ion-fluid calculation [Eq. (7)] does not provide insights into how density and/or temperature deviations from average-ion-fluid models directly impact the reaction rate ratios. Figure 9 provides a way to visualize these impacts by comparing reaction rate ratios assuming an averaged density profile but allowing ion temperature decoupling [Eq. (5), (orange)] and reaction rate ratios assuming an averaged temperature profile but allowing different density profiles [Eq. (6), (green)]. These FPION reaction rate ratios are normalized to the average-ion calculation [Eq. (4), (black horizontal line at 1.0)].

Ion species separation—specifically a higher $^3\text{He}/T$ fuel ratio as seen in Figs. 6(c) and 7(b)—has the most direct impact on the $D^3\text{He}/DT$ reaction rate ratio [Fig. 9(a)] in FPION simulations. As also seen in Fig. 7(d), near the bang time ($t \sim 0.7$ ns), the temperature difference between ^3He and T ions is small, minimizing the impact on the $D^3\text{He}/DT$ reaction rate ratio.

Both ion species separation and ion temperature decoupling contribute to the higher $D^3\text{He}/DD$ reaction rate ratio [Fig. 9(b)] in FPION simulations. The higher $^3\text{He}/D$ fuel ratio near the bang time [$t \sim 0.7$ ns, Figs. 7(a) and 6(c)] contributes to the higher $D^3\text{He}/DD$ reaction rate ratio. At the same time, the higher ^3He ion temperature (relative to D) near the bang time [$t \sim 0.7$ ns, Figs. 7(c) and 6(d)] also contributes to the higher $D^3\text{He}/DD$ reaction rate ratio in the FPION simulations.

Finally, differences in both ion densities and temperatures are expected to slightly change the DT/DD reaction rate ratio as compared to the average-ion calculation in the FPION simulations, but these effects are small [Fig. 9(c)].

V. CONCLUSION

In conclusion, multiple reaction histories simultaneously measured using the PXTD in shock-driven implosion experiments with $D^3\text{He}$ or $D^3\text{He}$ (with trace T) gas fills are used to probe plasma conditions during the shock phase of ICF implosions. These measurements (yields, ion temperatures, bang times, burnwidths, and time-resolved reaction rate ratios) are compared against average-ion DUED and kinetic-ion FPION simulations. On average, FPION is able to better match the measured yields, burnwidths, and timing differences between nuclear bang times (although the FPION-simulated timing differences are still smaller than measured). However, DUED is able to better match the measured ion temperatures. Differences between FPION and data may be a limitation of the hybrid hydro-kinetic approach used by FPION, which relies on initial conditions and trajectories from average-ion-fluid simulations.

This work shows that for relatively hydrodynamiclike implosions ($\langle N_K \rangle \sim 0.3$), average-ion simulations are able to reasonably match

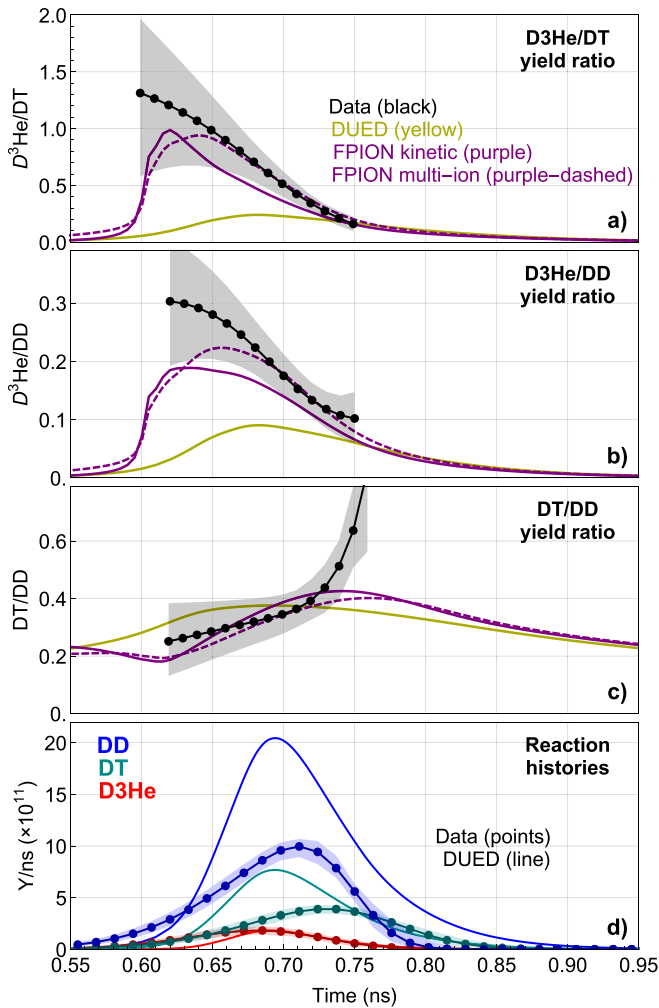


FIG. 8. (a) $D^3\text{He}/DT$ reaction rate ratio, (b) $D^3\text{He}/DD$ reaction rate ratio, and (c) DT/DD reaction rate ratio as a function of time, as measured by PXTD (black data), as calculated from DUED [yellow, Eq. (4)], as calculated from FPION using kinetic calculations (purple), and as calculated from FPION using multi-ion calculations [purple-dashed, Eq. (7)]. The PXTD-measured reaction rate ratio (black data) is shown with the shaded region denoting the uncertainty. In (d), PXTD-measured (data) and DUED-simulated (line) DD (blue), DT (teal), and $D^3\text{He}$ (red) reaction histories are shown as a timing reference.

some observables like yields and ion temperatures as well as burnwidths, but not other observables like reaction history timing differences. This is analogous to the conclusion in the study by Rosenberg *et al.*,³⁶ which found that additional kinetic physics are needed to explain the measured spatially resolved burn profiles in similar shock-driven implosions.

Shock-driven implosions play an important role in understanding how kinetic and multi-ion physics during the shock phase affect implosion performance later during compression when implosion conditions are much more hydrodynamic. For example, during compression, species separation²² (imprinted from separation during the shock phase), and temperature decoupling¹⁸ have been predicted in kinetic-ion simulations. Very hydrodynamic shock-driven implosions³⁷ have been tested at the National Ignition Facility (NIF) although NIF

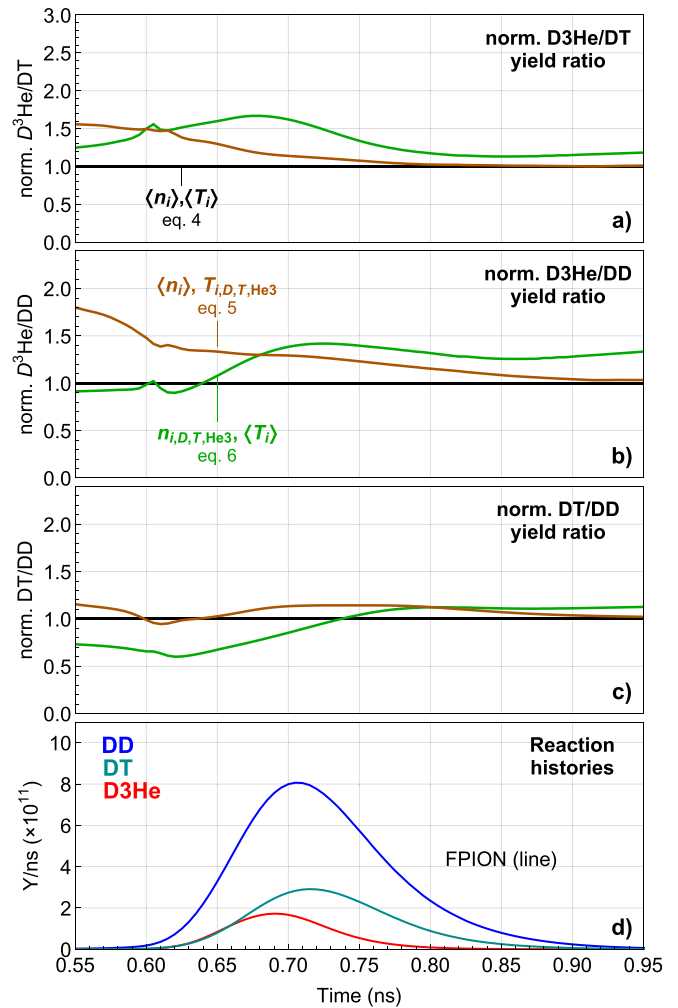


FIG. 9. (a) $D^3\text{He}/DT$ reaction rate ratio, (b) $D^3\text{He}/DD$ reaction rate ratio, and (c) DT/DD reaction rate ratio as a function of time, normalized to the average-ion expectation. Reaction rate ratios are calculated through different reduction of the FPION profiles: the average-ion expectation [$\langle n_i \rangle, \langle T_i \rangle$], black horizontal line at 1.0, Eq. (4), the average-density expectation [$\langle n_i \rangle, T_D, T_T, T_{^3\text{He}}$], orange, Eq. (5), and the average-temperature expectation [$n_{i,D}, n_{i,T}, n_{i,^3\text{He}}, \langle T_i \rangle$], green, Eq. (6)]. In (d), FPION-simulated (line) DD (blue), DT (teal), and $D^3\text{He}$ (red) reaction histories are shown as a timing reference.

lacks a PXTD-type instrument. Future work will focus on probing very kinetic ($N_K \geq 1$) and very hydrodynamic ($N_K \ll 1$) plasma conditions using multiple reaction histories, as well as signatures of kinetic effects (such as thermal decoupling between different ion species) in astrophysical settings.

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APPENDIX: DATA AND SIMULATION TABLE

TABLE I. Yields, ion temperatures, bang times, and burnwidths as measured in the experiments and as simulated by DUED and FPION. The uncertainties in the DD, D³He, and DT yields are UED and FPION. The uncertainties in the DD, D_{he} average-ion expect³He, and DT ion temperatures are 0.5 keV, ±2 keV, and ±0.5 keV, respectively. The absolute uncertainty in the bang times (BTs) is ±50 ps. The relative uncertainty between the bang times is ±10 ps (except for shots 70 562, 71 541, and 71 542, with a relative uncertainty of ±20 ps). The uncertainty in the burnwidths (BW) is 15%. OD and ΔR are the outer diameter and shell thickness of the SiO₂ targets, respectively. Information for shot 82 613–82 616 is adapted with permission from Sio *et al.* Phys. Rev. Lett. **122**, 035001 (2019). Copyright 2019 American Physical Society.

Shot	Target						DD				D ³ He				DT			
	OD μm	ΔR μm	Frac. D	Frac. ³ He	Frac. T	ρ mg/cc	Yield	T _i keV	BT ps	BW ps	Yield	T _i keV	BT ps	BW ps	Yield	T _i keV	BT ps	BW ps
50%–50% D ³ He																		
70 562	842	2.2	0.48	0.52	0	2.1	2.3 × 10 ¹⁰	12.3	754	114	4.0 × 10 ¹⁰	14.0	704	84				
71 541	866	2.1	0.51	0.49	0	2.0	2.5 × 10 ¹⁰	13.1	754		3.0 × 10 ¹⁰	14.0	718	105				
71 542	851	2.1	0.50	0.50	0	2.0	2.7 × 10 ¹⁰	13.8	705	109	3.6 × 10 ¹⁰	15.0	648	94				
Experiment average							2.5 × 10 ¹⁰	13.1	738	112	3.5 × 10 ¹⁰	14	690	94				
DUED							6.8 × 10 ¹⁰	13.6	656	117	7.4 × 10 ¹⁰	14.5	654	85				
FPION							2.2 × 10 ¹⁰	10.7	694	119	3.2 × 10 ¹⁰	15.1	675	88				
50%–50% D ³ He, trace T																		
82 613	865	2.7	0.51	0.48	0.007	2.0					3.9 × 10 ¹⁰	13.0	755	108	1.7 × 10 ¹¹	14.9	809	121
82 614	889	2.7	0.50	0.49	0.007	2.0	4.0 × 10 ¹⁰	11.0			5.0 × 10 ¹⁰	15.4	787	104	2.0 × 10 ¹¹	11.6	841	111
82 615	855	2.7	0.50	0.50	0.007	2.0	3.8 × 10 ¹⁰	10.7			5.0 × 10 ¹⁰	13.5	789	96	1.9 × 10 ¹¹	10.5	831	104
82 616	864	2.7	0.50	0.50	0.007	2.0	3.7 × 10 ¹⁰	11.1			3.7 × 10 ¹⁰	11.9	840	101	2.0 × 10 ¹¹	10.9	876	102
Experiment average							3.8 × 10 ¹⁰	10.9			4.4 × 10 ¹⁰	13.4	793	102	1.9 × 10 ¹¹	12.0	839	110
DUED							1.2 × 10 ¹¹	12.1			1.2 × 10 ¹¹	14.1	810	56	6.0 × 10 ¹¹	12.6	820	72
FPION							2.9 × 10 ¹⁰	9.5			3.2 × 10 ¹⁰	13.3	834	77	1.7 × 10 ¹¹	10.1	858	103
90%–10% D ³ He																		
82 731	845	2.5	0.88	0.12	0	3.4	1.3 × 10 ¹¹	10.3	750	102	1.5 × 10 ¹⁰	10.2	691	94				
82 734	889	2.4	0.90	0.10	0	3.3	1.8 × 10 ¹¹	11.3	791	89	2.3 × 10 ¹⁰	10.6	741	79				
82 735	865	2.4	0.88	0.12	0	3.4	1.4 × 10 ¹¹	11.8	728	80	2.1 × 10 ¹⁰	12.0	684	82				
82 745	877	2.6	0.89	0.11	0	3.4	1.7 × 10 ¹¹	11.5	734	95	2.2 × 10 ¹⁰	11.4	693	81				
Experiment average							1.5 × 10 ¹¹	11.2	751	92	2.0 × 10 ¹⁰	11	702	84				
DUED							2.3 × 10 ¹¹	9.6	774	105	1.3 × 10 ¹⁰	10.2	765	80				
FPION							1.6 × 10 ¹¹	8.9	789	114	1.8 × 10 ¹⁰	12.2	771	89				
90%–10% D ³ He, trace T																		
87 034	859	2.2	0.89	0.11	0.0009	3.1	1.2 × 10 ¹¹	9.6	769	109	2.0 × 10 ¹⁰	9.1	731	113	5.4 × 10 ¹⁰	8.9	785	128
87 036	851	2.2	0.89	0.11	0.0009	3.1	1.2 × 10 ¹¹	9.6	795	113	2.2 × 10 ¹⁰	11.5	754	111	5.3 × 10 ¹⁰	10.2	811	128
Experiment average							1.2 × 10 ¹¹	9.6	782	111	2.1 × 10 ¹⁰	10.3	743	112	5.3 × 10 ¹⁰	9.6	798	128
DUED							2.3 × 10 ¹¹	10.0	745	93	1.5 × 10 ¹⁰	10.5	738	83	8.0 × 10 ¹⁰	10.4	745	93
FPION							1.1 × 10 ¹¹	8.6	763	112	1.2 × 10 ¹⁰	11.8	747	85	4.2 × 10 ¹⁰	9.2	770	104

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